

Appendix A. Supplementary material

File: `user-guide.pdf`

Figure A.15: User guide for *Nektar++* detailing compilation, installation, input format and usage, including examples.

File: `insitu.zip`

Figure A.16: *Nektar++* input files for simulating flow past a cylinder at $Re = 80$ using `IncNavierStokesSolver`. This example uses the HDF5 input format described in Section 3.1 and the in-situ processing facilities of Section 3.2 to generate an animation of the vorticity field and show the von Kármán vortex shedding in this regime.

File: `adaptiveOrder.zip`

Figure A.17: *Nektar++* input files for simulating flow over a NACA0012 wing at $Re = 50,000$ using `IncNavierStokesSolver`. This example uses an adaptive-in-time polynomial order described in Section 4.2 to increase efficiency of the simulation when compared to a spatially-constant polynomial order.

1 File: wavyWing.zip
2 Figure A.18: *Nektar++* input files for simulating flow over a wavy NACA0012
3 wing at $Re = 1,000$ using *IncNavierStokesSolver*. This example uses the
4 mapping technique described in Section 4.3 to perform simulations in a quasi-3D
5 setting.
6 File: acoustic.zip
7
8 Figure A.19: *Nektar++* input files for simulating the spinning vortex pair using
9 the *AcousticSolver* of Section 5.2 at a polynomial order of $P = 5$, accelerated
10 using the *Collections* library described in Section 3.3.
11 File: meshGen.zip
12
13 Figure A.20: *NekMesh* input files for a NACA0012 aerofoil section and T106C
14 turbine blade geometry outlined in Section 5.1.
15
16 File: vivCylFlow.zip
17
18 Figure A.21: *Nektar++* input files for simulating flow over a flexible cylinder
19 $Re = 3,900$ using the *IncNavierStokesSolver*. This example uses the the
20 thick strip model outlined in Section 5.3 to reduce computational cost against a
21 full 3D simulation.
22 File: shockBL.zip
23
24 Figure A.22: *Nektar++* input files for simulating a shock boundary-layer inter-
25 action test case, at a Reynolds number $Re = 10^5$, Mach number $Ma = 2.15$ and
26 shock angle $\beta = 30.8^\circ$ as outlined in Section 5.4.